| Candidates must complete this page and then give this cover and their final version of the extended essay to their supervisor. |  |  |
| :--- | :--- | :--- |
| Candidate session number |  |  |
| Candidate name |  |  |
| School number |  |  |
| School name |  |  |
| Examination session (May or November) | MA Y | Year |

Diploma Programme subject in which this extended essay is registered: PHYS ICS
(For an extended essay in the area of languages, state the language and whether it is group 1 or group 2.)

Title of the extended essay: INVESTIGATING A WATER ROCKET

## Candidate's declaration

This declaration must be signed by the candidate; otherwise a grade may not be issued.
The extended essay I am submitting is my own work (apart from guidance allowed by the International Baccalaureate).

I have acknowledged each use of the words, graphics or ideas of another person, whether written, oral or visual.

I am aware that the word limit for all extended essays is 4000 words and that examiners are not required to read beyond this limit.

This is the final version of my extended essay.

Candidate's signature:


Date: 13.01 .2012 Date: 13.01 .2012

## Supervisor's report and declaration

The supervisor must complete this report, sign the declaration and then give the final version of the extended essay, with this cover attached, to the Diploma Programme coordinator.

## Name of supervisor (CAPITAL letters)

Please comment, as appropriate, on the candidate's performance, the context in which the candidate undertook the research for the extended essay, any difficulties encountered and how these were overcome (see page 13 of the extended essay guide). The concluding interview (viva voce) may provide useful information. These comments can help the examiner award a level for criterion K (holistic judgment). Do not comment on any adverse personal circumstances that may have affected the candidate. If the amount of time spent with the candidate was zero, you must explain this, in particular how it was then possible to authenticate the essay as the candidate's own work. You may attach an additional sheet if there is insufficient space here.

The topic was determined by the candidate's fascination by rockets. His extensive background study on rockets in general had been an ongoing engagement, the essay was just one further impetus. The water rocket provided an experimentally approachable form of rocket propulsion that lent itself to effective treatment of a research question. In the preparatory reading phase the candidate had to face internet based sources being diverse in quality. He needed to reject some of them as scientifically unreliable, but "serious" sources provided conflicting information, too. In our discussions, the candidate demonstrated a sound critical approach to such sources.
The topic required the synthesis of mechanics and thermal physics and areas beyond the DP syllabus (quantitative treatment of an adiabatic change, equation of continuity, Bernoulli's law). In all this theoretical background, as well as in homogeneous and inhomogeneous differential equations, he was tutored by friends outside the school.
As reflected by my interviews with him, he successfully developed an understanding in these areas.
The candidate's writing is somewhat hard to follow (same is the case with his tests and lab reports): He cannot be convinced that he should not talk about something until he defined/stated what it was. It needed considerable effort on my part to question him about all the content of the essay, and gain evidence that he thoroughly understands everything. He does. (The final version of the essay became a lot more readable than the first draft was.)

This declaration must be signed by the supervisor; otherwise a grade may not be issued.
I have read the final version of the extended essay that will be submitted to the examiner.
To the best of my knowledge, the extended essay is the authentic work of the candidate.
I spent 4 hours with the candidate discussing the progress of the extended essay.

Supervisor's signature:
Date: 1 March 2012

## Assessment form (for examiner use only)

Candidate session number

Achievement level

| Criteria | Examiner 1 | maximum | Examiner 2 | maximum | Examiner 3 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| A research question | 2 | 2 | 2 | 2 |  |
| B introduction Thewry is warls pace | 1. | 2 | 2 | 2 |  |
| C investigation | 4. | 4 | 4 | 4 |  |
| D knowledge and understanding | 14. | 4 | 4 | 4 |  |
| E reasoned argument | 4 | 4 | 4 | 4 |  |
| F analysis and evaluation | 3 | 4 | 4 | 4 |  |
| G use of subject language | 4 | 4 | 4 | 4 |  |
| H conclusion (uamsolan ispus? |  | 2 | 1 | 2 |  |
| 1 formal presentation | 4 | 4 | 4 | 4 |  |
| $J$ abstract | 2 | 2 | 2 | 2 |  |
| K holistic judgment on of the ravy bist I | 4 | 4 | 4 | 4 |  |
| Total out of 36 | $0$ |  |  |  |  |

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## EXTENDED ESSAY

## Investigating a water rocket

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## Name:

## Session number:

## School:

Subject: Physics
Supervisor's name:
Word counts: 3990

## Abstract

A self-made water rocket is an inverted plastic bottle which is filled with a fixed amount of pure water. Air is pumped inside it until the pressure of the trapped air is large enough to be able to push the plug out.

The motion of the water rocket was investigated experimentally, with the use of a highspeed camera and a video analysis software. The purpose of the investigation was to determine the optimal amount of water (fuel) needed for the rocket to fly as high as possible, and to provide the explanation of the results based on the principles of physics.

The motion of the water rocket can be divided into three stages: the rocket propelled by the thrust of the ejected water, the further rise of the empty rocket to the highest point of the trajectory and the fall of the rocket. A mathematical model was set up for each of the first two stages, and the values of rising times, velocities and heights calculated from the model were compared to the experimental results.

According to several articles and water rocket simulators the ideal amount of water is about one third or between $40 \%$ and $50 \%$ of the total capacity of the body of the inverted plastic bottle. It means that the water rocket will fly the highest if one third or $40 \%$ to $50 \%$ of the bottle is occupied by water. The statements were neither justified by the model nor the experiment. However, the model and the experimental results fit well, which means the model is reliable, therefore the statements are only acceptable as a rough approximation.

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## I. InTRODUCTION

Ihave always been interested in space shuttles so I did some investigation to reveal the physics behind the process of using rockets to launch the space shuttle. Rockets apply Newton's second and third law by creating thrust and do not require external forces but fuel inside them to be launched. A water rocket applies the same physical laws and it is easier to launch than a space shuttle, moreover, a water rocket is very much similar to a NASA rocket [1]. A water rocket is an inverted plastic bottle which is filled with a fixed amount of water. Air is pumped inside it until the pressure of the trapped air is large enough to push the plug out. The thrust of the water squirting out propels the rocket (Figure 2). However, no matter how much fuel is filled into the water rocket, it cannot be launched high enough to set it in orbit. han bun

## Research Question:

How does the maximum height that the water rocket can reach change with the variation of the initially filled amount of water?

It seems reasonable that there is an optimal amount, since in the case of not filling the bottle enough, the rocket will lack fuel. In the other case when the bottle is overfilled, the rocket will be too heavy and not uses up all of its fuel. According to several articles and water rocket simulators the ideal amount of water is about one third $[2,3,4]$ or $40 \%$ to $50 \%$ $[5,6]$ of the total capacity of the body of the rocket. It means that the water rocket will fly the highest if one third or $40 \%$ to $50 \%$ of the bottle is occupied by water.

The goal of my investigation was to find out which hypothesis is proved or disproved by experiment, and to justify the results by the principles of physics.


Figure 1: [13] Atlantis Space Shuttle, last Launch by NASA in 2011


Figure 2: The investigated water rocket, first launch by me in 2011


## a) Constructing a water rocket

In the experiment one of the simplest versions of a water rocket was made. This particular type of water rocket is a simple PET plastic bottle that has two heads. Therefore, there needs to be two PET bottles. One bottle's top is going to be the nose cone; which is attached to the other bottle's bottom (Figure 3). This enhances the stability of the rocket and reduces air drag while it flies.


Figure 3: The construction of the water rocket

In the experiment, the body of the rocket was an old 2-litre coke bottle. Nowadays, to protect the environment only thin walled PET bottles are produced. To make the rocket's flight more stable the harder or older type of bottles should be used. ${ }^{1}$ During the experiment, it was experienced that the flight of the rocket was not really straight so a little mass (a screw) was placed in the nose cap in order to straighten the flight. Just like the darts that have a little mass on the nose to make their flight more stable. Moreover, if the mass of the rocket is to be varied then nuts can be put on the screw to make it heavier.

To operate the rocket, at first, a fixed amount of water has to be filled in and then air is continuously pumped in it until no more can be added. This means that the internal pressure from the bottle is great enough to push out a plug and so, the water. Finally, the rocketrises due to the ejection of water and the trapped air. However, the plug is not a regular cork since not only water but also air has to be added into the bottle. This is why the cork is drilled longitudinally and centrally to be able to insert a

[^0]bicycle tube valve. The cork was too long for the valve so it had to be shortened with a knife. This method allows adding air into the bottle without the water flowing out.


Figure 4: The stopper used in the mouth of the rocket in the experiment

Finally, to pump air, the valve has to be connected to an air supply. Once the air is pumped in, due to the expansion of the compressed air the cork is pushed out which will result in the acceleration of the rocket upwards. The easiest and cheapest way to pump in air is to use bicycle pump or car tire foot pump. It is also important that the pump has to have a pressure meter for it should be known with what initial pressure it is launched. In this experiment, a bicycle pump was used which was equipped with a pressure gauge with the smallest scale unit of one fifth of a bar. This is why the measurement of pressure was the least precise relative to other quantities measured in the experiment.

## b) Launching the water rocket

The launcher has two important parts. The wooden base supports all the other components and provides stability. The launch tube: helps the rocket fly vertically, especially at the beginning of the launch. The launch tube was cut from a PVC tube, fixed to the base with wires (Figure 5).


Figure 5: The launch pad of the water rocket

## III. THE EXPERIMENT

## a) The technicall data of the water rocket

For measuring the diameter of the body of the rocket and the diameter of the nozzle a caliper was used. To measure the volume of the body of the rocket, the empty bottle was filled with water and then that amount of water was poured into a measuring cylinder which had centiliter divisions. The mass of the empty rocket was determined by putting the rocket on a kitchen scale on which the smallest unit was one gram.

The volume of the body of the rocket $V_{R}: 2.3$ litre


Figure 6: The initial parameters of the water rocket

- Largest diameter and the cross-sectional area of the rocket:

$$
d_{L}=(10.10 \pm 0.03) \mathrm{cm} \text { and } A_{L}=(80.1 \pm 0.5) \mathrm{cm}^{2}
$$

- Diameter and the cross-section of the nozzle:

$$
d_{m}=(20.0 \pm 0.2) \mathrm{mm} \text { and } A_{m}=(3.14 \pm 0.06) \mathrm{cm}^{2}
$$

- Volume of the body of the rocket:

$$
V_{R}=(2300 \pm 5) \mathrm{ml}
$$

- Mass of the empty rocket :

$$
m_{R}=(225 \pm 1) \mathrm{g}
$$

Note: The errors of the measured values are the half of the smallest scale unit but if the measurement is dubious then larger error should be used.

In the case of the error of the cross-sectional areas the error percentages are added. For instance, $A_{m}=\left(\frac{d_{m}}{2}\right)^{2} \times \pi$ will have an error of $2 \%$ because $d_{m}$ has $1 \%$ error and its square will have an error of $2 \times 1 \%=2 \%$.

## b) What was measured?



Eleven different amounts of water were used. To match the hypothesis about $\frac{1}{3}$ or $40 \%$ to $50 \%$ volume, the volume of the rocket was divided into twelfths and the multiples of it were measured with the same volume meter as above, with centiliter divisions. The fractions of the body of the rocket filled with water are shown:

| $\frac{0.0}{12}$ | $\frac{2.0}{12}$ | $\frac{2.5}{12}$ | $\frac{3.0}{12}$ | $\frac{3.5}{12}$ | $\frac{4.0}{12}$ | $\frac{4.5}{12}$ | $\frac{5.0}{12}$ | $\frac{5.5}{12}$ | $\frac{6.0}{12}$ | $\frac{8.0}{12}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 0.17 | 0.21 | 0.25 | 0.29 | 0.33 | 0.38 | 0.42 | 0.46 | 0.50 | 0.67 |

Table 1: The ratios of the water and the body of the rocket that were examined

The movement of the water rocket can be divided into three stages. The first stage is when the rocket ejects water and accelerates to its maximum velocity. This stage ends when all the water has left the bottle, then, the second stage begins; in which the rocket still goes up without ejecting any water and then it stops due to air drag and gravitational force. The last phase is when the rocket falls down to the ground. The investigation only deals with the first two stages.

## i. The application of the camera

The most convenient way to analyze the motion of the water rocket is to use a high-speed camera, because the rocket ejects all of its water in tenth of seconds. Mostly, ordinary camcorders record 30 frames per second (fps), while a high-speed camera can record much more frames. In the experiment, a Casio Zr100 type of camera was used which was able to record in $1000 \mathrm{fps}, 480 \mathrm{fps}$, and 240 fps . With the help of this camera, the displacement of the rocket with respect to time was determined. Although the more frames it uses, the easier it can be analyzed, however, using slow motion recording mode will decrease the quality of the video. Therefore, it was suitable to use the 240fps mode. Unfortunately, only the first stage of the rocket's movement was recorded because at larger heights the error of perspective is increasing.

It should also be noted that the camera should be used on a stand; otherwise the camera will be moving and it will affect the measurements in the video analyzer.

Figures 7 and 8 show the time of ejection of the rocket; it can be seen that the water runs


Figure 9 shows another launch's every fifth frame with the very top of the rocket marked with a red circle.

ii. The analysis of the recorded video

The recorded video was analyzed by a video analyzer program, Logger Pro 3.8.4. With the help of this program, the maximum velocity of the rocket as well as the time taken to eject all of its water was determined. During this experiment every second or fifth frame of the video was examined (Figure 10).


Figure 10: The method of examining every second frame in Logger Pro 3.8.4. The red line is a reference distance which is 0.58 m .

Note: At larger initial water amount, collecting data points from every fifth frame allowed a nicer graph.

## iii. The initial pressure

The pressure of air pumped in the bottle was read from the pressure meter while continuously adding air into the rocket. The maximum initial pressure is shown on the pressure meter when the plug in the mouth of the rocket has just been pushed out. This variable had to be controlled by inserting the cork into the mouth of the bottle with the same pushing force and same circumstances. For instance, if the cork was initially inserted when it was dry then before all the launches the cork as well as the inner mouth of the bottle should be dried. Unfortunately, the initial pressure could not be controlled very well, the initial pressures had large deviations.

## iv. The maximum height

The maximum height reached by the rocket was measured by using a thread. The spool was placed right under the rocket and the end of the thread was fastened to the mouth of the rocket. Therefore, when the rocket rises upwards it pulls the thread after itself until it reaches the highest point of its trajectory then it falls down. Afterwards, the pulled out thread was measured by measuring tape. It would be more comfortable to determine the height from the video but as mentioned before, only the first stage could be recorded since the rocket still goes upwards after it has ejected all the water and it gets out of view of the camera.

Figure 11: The set up of the height measuring equipment


Figure 12: The determination of the maximum height reached by the rocket

## c) The results of the measurements

Figures 13 and 14 produced by Logger Pro, are examples to illustrate the result of collecting data points from every fifth and second frame from a recorded video.
a)

b)


Figure 13: Shows (a) the displacement and (b) the velocity of a 575 ml rocket with respect to time when collecting data from every fifth frame
a)

b)


Figure 14: Shows (a) the displacement and (b) the velocity of a 383 ml rocket with respect to time when collecting data from every second frame

$$
\begin{aligned}
& \text { fresh sum cull } \\
& \text { fracher of line wohch It } \\
& \text { carlo he a good dee (to } \\
& \text { cauphes fricts fin root }
\end{aligned}
$$

The following table shows the average measured values of the experiment and the errors were the difference of the average and the measured value:

| The average initial pressure $p_{1}:(2.9 \pm 0.3)$ bar $^{2}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| The volume ratio of <br> the water and the <br> bottle | Initial water amount <br> $V_{0}(\mathrm{ml})$ | Measured <br> maximum <br> velocity $v_{\text {max }}$ <br> $\left(\mathrm{ms}^{-1}\right)$ | Measured <br> time of <br> ejection of <br> water $t_{t}(\mathrm{~s})$ | Measured <br> maximum <br> error: $\pm 5 \mathrm{ml}$ <br> $(\mathrm{m})$ |
| error: $\pm 1.1 \mathrm{~ms}^{-1}$ | error: 0.003 | error: $\pm 0.5 \mathrm{~m}$ |  |  |$|$| $2.0 / 12=0.17$ | 383 | 20.1 | 0,070 | 16.2 |
| :---: | :---: | :---: | :---: | :---: |
| $2.5 / 12=0.21$ | 479 | 22.5 | 0,088 | 18.6 |
| $3.0 / 12=0.25$ | 575 | 25.0 | 0,088 | 19.7 |
| $3.5 / 12=0.29$ | 671 | 24.4 | 0,142 | 21.9 |
| $4.0 / 12=0.33$ | 767 | 26.0 | 0,129 | 22.8 |
| $4.5 / 12=0.38$ | 863 | 25.5 | 0,167 | 23.1 |
| $5.0 / 12=0.42$ | 958 | 25.1 | 0,186 | 23.6 |
| $5.5 / 12=0.46$ | 1054 | 24.1 | 0,222 | 21.9 |
| $6.0 / 12=0.50$ | 1150 | 20.0 | 0,267 | 17.8 |
| $8.0 / 12=0.67$ | 1533 | 9.8 (not exact) | - | 8.5 |

Table 2: Shows the results of the measured variables in the experiment

The values of $v_{\max }$ and $t_{t}$ at the $\frac{8.0}{12}$ water amount are not exact for the rocket contained too much water and the camera could not record the whole phase of ejection.


[^1]
## IIII. ANALYZING AND MODELING THE PHASES OF THE ROCKET'S MOVEMENT

## a) The phase when the rocket accelerates

camener

At first, to estimate the rocket's maximum height for a particular amount of water, the maximum velocity should be obtained. Theoretically, the acceleration of the rocket ends when the fuel runs out which means the rocket reaches its maximum speed at the end of the first stage.

## i. Expressing the velocity of the water and the time of ejection of the water

While the air is continuously pumped into the closed bottle, the pressure of the trapped air is increasing. Thus, the cork will be pushed out when the sum of the forces of the pressure of the compressed air and the hydrostatic pressure of the water acting on the inner surface of the cork is greater than that of the atmospheric pressure acting on the external end of the cork and the maximum of the static friction between the side of the cork and the wall of the mouth of the bottle together (Figure 15).


Figure 15: The water rocket before it is launched

After the cork is pushed out, the compressed air expands really fast and pushes out the total or only certain amount of water from the bottle. The process takes place really fast (e.g.:0.125 s) which means it is a good approximation to assume that the gas and its surroundings do not exchange heat. This process is called adiabatic expansion, and the Poisson equation relates the different states of the gas $[7,8,10]$ :

$$
\begin{equation*}
p_{1} V_{1}^{\gamma}=p(t)[V(t)]^{\gamma} \tag{1}
\end{equation*}
$$

where $p_{1}, V_{1}$ and $p(t), V(t)$ are the pressure and the volume initially, and at a later time $t$. Now $\gamma=1.4$ because air mostly consists of diatomic gas [7, 10].

Truly, the water in the bottle does not necessarily leave completely. This is why there are two cases. Provided that the initial water level is not high and enough air is added into the bottle, the compressed air will expand to greater volume than the volume of the rocket.
 Only this way can the compressed air decrease its pressure to the atmospheric pressure. In this case, all the amount of water will leave the bottle by the end of the ejection phase (case 1) [8].

In the event of loading too much water or if the compressed air's pressure is low enough, the air will expand to lower volume than the volume of the rocket. In this way, the air will not push all the water out and the rocket will fly with the remaining amount of water (case 2). In the experiment, at the largest amount of water ( 1.533 litre), the rocket still had water inside it after it landed. In order to launch the rocket as high as possible, the appropriate amount of water should be filled in where the rocket just uses up all the fuel. In this way, case 1 should be examined.

## THE FIRST CASE

The water is continuously leaving the bottle, thus, applying the law of continuity for incompressible liquids [8, 10]: the same volume of water is pushed downwards by the air, as the volume coming out.


Figure 16: The water rocket when it is being launched

Owing to the laws of continuity and energy conservation, the acting pressures and speeds at the two ends of the water column at a time $t$ are connected by Bernoulli's principle [7, 8, 10]:

$$
p(t)+\rho_{w} g h(t)+\frac{1}{2} \rho u_{0}(t)^{2}=p_{a}+\rho_{w} g h_{2}(t)+\frac{1}{2} \rho_{w} u(t)^{2}
$$


where $p(t)$ and $p_{a}=10^{5} P a$ are the pressures of the compressed air at time $t$ and the pressure of the atmosphere, $\rho_{w}=1000 \frac{\mathrm{~kg}}{\mathrm{~m}^{3}}$ is the density of the water, $h(t), h_{2}(t)$ are the heights of the water surfaces, and $u_{0}(t), u(t)$ are the velocity of the water relative to the bottle at the water surfaces inside and outside of the bottle at time $t$.

Since the inner cross-sectional area is much greater than that of the mouth, it can be assumed that the velocity of the water $u_{0}(t)$ is $0 \mathrm{~ms}^{-1}$. Actually, the inner cross sectional area is $80.1 \pm 0.5$, and the mouth is 3.1 which is not really negligible, but considering the inaccuracy of the pressure reading this step is justified.

Since the hydrostatic pressures $\rho_{w} g h_{1}(t)$ and $\rho_{w} g h_{2}(t)$ are really small ${ }^{3}$ compared to the pressures $p(t)$ and $p_{a}$, they can also be neglected. So the simplified equation is:

$$
p(t)=p_{a}+\frac{1}{2} \rho_{w} u(t)^{2}
$$

Hence, with the right arrangements and the omission of the mentioned quantities, the velocity of the water $u(t)$ relative to the rocket at a given time $t$ is [8]:

$$
\begin{equation*}
u(t)=\sqrt{\frac{2\left(p(t)-p_{a}\right)}{\rho_{w}}} \tag{2}
\end{equation*}
$$

This is a simpler result than that in [7].
The pressure at time $t$ can be expressed by applying equation (1). So, the initial velocity of the water $u_{1}$ can be obtained by substituting the measured initial pressure

$$
u_{1}=\sqrt{\frac{2\left(p_{1}-p_{a}\right)}{\rho_{w}}}
$$

[^2]Consider time $t$, when all the water went out. Therefore, using equation (1) $V(t)$ equals the volume of the rocket $V_{R}$, and the pressure at the end of the first stage $p_{2}$ is:

$$
\begin{equation*}
p_{2}=\left(\frac{V_{1}}{V_{R}}\right)^{\gamma} p_{1} \tag{3}
\end{equation*}
$$

Note: $V_{1}=V_{R}-V_{0}$

Hence, the final velocity $u_{2}$ of the water coming out can be calculated by substituting this value of the final pressure $p_{2}$ in (2). For instance, for $V_{0}=0.383$ litre,

$$
p_{2}=\left(\frac{1.917}{2.300}\right)^{1.4} \times 2.9=2.3 \mathrm{bar} \quad u_{2}=\sqrt{\frac{2(2.3-1) \times 10^{5}}{1000}}=16.1 \mathrm{~ms}^{-1}
$$

After obtaining the initial and the final velocity of the water in the ejection phase, an estimation of average velocity can be used by taking the average of the initial and final velocity of the water, which means the estimation assumes a uniform acceleration.

Another assumption should be considered: the water column that comes out, which is exactly the volume of the initially used water $V_{0}$, can be regarded as a cylinder which base is the cross-section of the mouth of the bottle, $A_{m}$.


Figure 17: The equation of continuity: the water leaving the rocket has a form of a cylinder

Where $V_{0}=A_{m} \bar{u} t_{t}, \bar{u}=\frac{u_{1} \pm u_{2}}{2}$ and $t_{t}$ is the time taken to eject all the water. In this way, the time taken for the rocket to push all the water out can be expressed as:


## The relative velocity and the time of ejection of the water

The following table compares the calculated values based on the above formulae to the measured values taken from table 2:

Table 3: Shows the variables needed to determine the calculated value of the time of ejection of water

| Initial parameters |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Average initial pressure $p_{1}:(2.9 \pm 0.3)$ bar |  |  | Initial relative water velocity$u_{1}=(19.5 \pm 2.0) \mathrm{ms}^{-1}$ |  |  |  |
| Cross-sectional area of nozzle $A_{m}=(3.14 \pm 0.06) \mathrm{cm}^{2}$ |  |  |  |  |  |  |
| Volume ratio of water and the bottle | Amount of water $V_{0}(I)$ | Calculated values from model |  |  |  | Measured time $t_{t}(\mathrm{~s})$ |
|  |  | Final pressure $p_{2}$ (bar) | Final water velocity $u_{2}\left(\mathrm{~ms}^{-1}\right)$ | Average of $u_{1}$ and $u_{2}$, $\bar{u}\left(\mathrm{~ms}^{-1}\right)$ | Ejection time $t_{t}(\mathrm{~s})$ |  |
| - | $\begin{aligned} & \text { error: } \\ & \pm 0.005 \end{aligned}$ | $\begin{aligned} & \text { error: } \\ & \pm \approx 10 \% \end{aligned}$ | $\begin{aligned} & \text { error: } \\ & \pm \approx 10 \% \end{aligned}$ | $\begin{aligned} & \text { error: } \\ & \pm \approx 10 \% \end{aligned}$ | $\begin{aligned} & \text { error: } \\ & \pm \approx 10 \% \end{aligned}$ | $\begin{aligned} & \text { error: } \\ & \pm 0.003 \end{aligned}$ |
| $2.0 / 12=0.17$ | 0.383 | 2.2 | 15.8 | 17.6 | 0.07 | 0.070 |
| $2.5 / 12=0.21$ | 0.479 | 2.1 | 14.8 | 17.1 | 0.09 | 0.088 |
| $3.0 / 12=0.25$ | 0.575 | 1.9 | 13.7 | 16.6 | 0.11 | 0.088 |
| $3.5 / 12=0.29$ | 0.671 | 1.8 | 12.6 | 16.0 | 0.13 | 0.142 |
| $4.0 / 12=0.33$ | 0.767 | 1.6 | 11.3 | 15.4 | 0.16 | 0.129 |
| $4.5 / 12=0.38$ | 0.863 | 1.5 | 10.0 | 14.8 | 0.19 | 0.167 |
| $5.0 / 12=0.42$ | 0.958 | 1.4 | 8.5 | 14.0 | 0.22 | 0.186 |
| $5.5 / 12=0.46$ | 1.054 | 1.2 | 6.8 | 13.1 | 0.26 | 0.222 |
| $6.0 / 12=0.50$ | 1.150 | 1.1 | 4.4 | 12.0 | 0.31 | 0.267 |
| $8.0 / 12=0.67$ | 1.533 | 0.6 | - | - | - | - |

Note: In the case of $p_{2}$, (3) is used to calculate the error. The error percentage of the values of the fraction and $p_{1}$ has to be added because the equation contains division and multiplication. Since the error of $V_{1}$ and $V_{R}$ are small compared to the error of $p_{1}$, it can be neglected so the error of $p_{2}$ is that of $p_{1}$, which is $10 \%$.

It can be seen that the model of the first case works up to 1.533 litre, where the final pressure becomes less than 1 bar and using equation (2) would make no sense ${ }^{4}$. From that $V_{0}$ onwards, case 2 prevails.


Figure 18: Shows the calculated and the measured value of the time of ejection of water at the initial pressure of 2.9 bar

ii. The motion of the rocket

To describe the motion of the rocket in this phase, Newton's second law is applied [7, 12]:

$$
F=\frac{d P}{d t}
$$

[^3]At a time $t$ after the launch the mass of the rocket is $m(t)$ and its velocity relative to the ground is $v(t)$. The total momentum of the system (bottle plus water inside) at time $t$ is:

$$
\begin{equation*}
P(t)=v(t) m(t) \tag{4}
\end{equation*}
$$

As water is continuously ejected from the bottle the mass of the rocket is continuously decreasing with respect to time, thus, the lost mass $\Delta m$ is a negative quantity. During a small time period, $\Delta t$ elapsed, the lost mass $|\Delta m|$ of water leaves the bottle with the velocity of $\bar{u}$ relative to the bottle, which then has a velocity of $-[\bar{u}-v(t)]$ relative to the ground. If the velocity of the rocket is $v(t)+\Delta v$ at time instant $t+\Delta t$. The total momentum of the rocket is:

$$
\begin{equation*}
p(t+\Delta t)=(v(t)+\Delta v)(m(t)+\Delta m), \tag{5}
\end{equation*}
$$

and the momentum of the ejected water is:

$$
\begin{equation*}
p_{w}(t+\Delta t)=-[\bar{u}-v(t)] \times|\Delta m|=\Delta m[\bar{u}-v(t)] \tag{6}
\end{equation*}
$$

Since, the momentum of the system after time $t+\Delta t$ is equal to the momentum of the rocket and the ejected water at that time, $\Delta P=p(t+\Delta t)+p_{w}(t+\Delta t)-P(t)$

If equations (4)(5)(6) are substituted into Newton's second law, after the simplifications the equation ${ }^{5}$

$$
\begin{equation*}
F=\lim _{\Delta t \rightarrow 0}\left(\frac{m(t) \Delta v+\Delta m \Delta v+\Delta m \bar{u}}{\Delta t}\right) \tag{7}
\end{equation*}
$$

is obtained. At small $\Delta t$, the term $\Delta m \Delta v$ can be neglected. Therefore equation (7) can be simplified as:

$$
F=\lim _{\Delta t \rightarrow 0}\left(\frac{\Delta v}{\Delta t} m(t)+\frac{\Delta m-\bar{u}}{\Delta t}\right)
$$

In this case, the external forces acting on the rocket are the gravitational force $-m(t) g$ and the air drag force $-C v(t)$, where $C$ is a constant. To express the velocity, only the gravitational force needs to be taken in account, because the air drag is small and it would not vary much ${ }^{6}$ the maximum velocity:

[^4]\[

$$
\begin{equation*}
-m(t) g=\frac{d v}{d t} m(t)+\frac{d m}{d t} \bar{u} \tag{8}
\end{equation*}
$$

\]

Hence, after solving the equation (8) the velocity at any time $t$ can be described by the Tsiolkovsky theorem [9]. However, a more complicated form (11) is used here than in [9], since this rocket had an initial velocity, for the video could not be examined exactly at the moment of the launch (because it could not be seen in the video), and the gravitational force was taken into account as well. ${ }^{7}$

$$
\begin{equation*}
v(t)=v_{0}+\bar{u} \ln \left[\frac{V_{0} \rho_{w}+m_{R}}{\left(V_{0}-\bar{u} A_{m} t\right) \rho_{w}+m_{R}}\right]-g(t) \tag{11}
\end{equation*}
$$

## $>$ Calculating the maximum velocity of the rocket

To determine the initial velocity $v_{0}$ of the rocket (11) should be fitted into the graph, made with Logger Pro (it shows data point from every fifth frame of a rocket with 767 ml water). The model only works until the end of the water ejection phase, which in this case is about $t_{t}=0.150 \mathrm{~s}$.


Figure 19: Shows the application of Tsiolkovsky theorem (11) on the measured values of the maximum velocity in Logger Pro 3.8.4

Given the constants of $\rho_{w}, m_{R}, A_{m}$, the program gives the values of the parameters $v_{0}=(3.366 \pm 0.4466) \mathrm{ms}^{-1}$ and $\bar{u}=(15.79 \pm 1.055) \mathrm{ms}^{-1}$ (denoted by $A$ in the red box), that is $v_{0}=(3.4 \pm 0.5) \mathrm{ms}^{-1}, \bar{u}=(16 \pm 1) \mathrm{ms}^{-1}$. The values of $t_{t}=0.150 \mathrm{~s}$ and $\bar{u}=(16 \pm 1) \mathrm{ms}^{-1}$ accord well with the calculated values of table 3 (shaded).

[^5]If more data points are taken (e.g.: every second frame is examined), which means a more detailed measurement is done then the initial velocity $v_{0}$ is much smaller (close to 0 ), because originally the rocket was launched at rest. Thus, in the model of the maximum velocity $v_{0}$ is neglected.

The values of table 4 below are obtained by substituting the values of $t_{t}$ (from table 3 ) into (11), using $v_{0}=0 \mathrm{~ms}^{-1}$.

Table 4: Shows the maximum velocity and the final pressure after it has ejected all of its water

| Initial parameters |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Mass of empty rocket $m_{R}=(0.225 \pm 1) \mathrm{g}$ |  |  | Density of water: $1000 \frac{\mathrm{~kg}}{\mathrm{~m}^{3}}$ |  |  |
| Average initial pressure $p_{1}:(2.9 \pm 0.3)$ bar |  |  | Area of nozzle $A_{m}=(3.14 \pm 0.06) \mathrm{cm}^{2}$ |  |  |
| Volume Ratio of water and bottle | Water (litre) | Final pressure in the rocket $p_{2}$ (bar) | Average of <br> $u_{1}$ and $u_{2}$, <br> $\bar{u}\left(\mathrm{~ms}^{-1}\right)$ | Calculated maximum velocity $v_{\text {max }}$ $\left(\mathrm{ms}^{-1}\right)$ | Measured maximum velocity ( $\mathrm{ms}^{-1}$ ) |
| - | $\begin{aligned} & \text { Error: } \\ & \pm 0.005 \end{aligned}$ | Error: $\pm \approx 10 \%$ | $\begin{aligned} & \text { Error: } \\ & \pm \approx 10 \% \end{aligned}$ | Error: $\pm \approx 10 \%$ | Error: $\pm 1.1$ |
| $2.0 / 12=0.17$ | 0.383 | 2.2 | 17.6 | 16.8 | 20.1 |
| $2.5 / 12=0.21$ | 0.479 | 2.1 | 17.1 | 18.7 | 22.5 |
| $3.0 / 12=0.25$ | 0.575 | 1.9 | 16.6 | 20.0 | 25.0 |
| $3.5 / 12=0.29$ | 0.671 | 1.8 | 16.0 | 20.8 | 24.4 |
| $4.0 / 12=0.33$ | 0.767 | 1.6 | 15.4 | 21.3 | 26.0 |
| $4.5 / 12=0.38$ | 0.863 | 1.5 | 14.8 | 21.4 | 25.5 |
| $5.0 / 12=0.42$ | 0.958 | 1.4 | 14.0 | 21.1 | 25.1 |
| $5.5 / 12=0.46$ | 1.054 | 1.2 | 13.1 | 20.3 | 24.1 |
| $6.0 / 12=0.50$ | 1.150 | 1.1 | 12.0 | 18.6 | 20.0 |
| $8.0 / 12=0.67$ | 1.533 | 0.6 (not exact) | - | - | 9.8 (not exact) |

Note: The errors were calculated with the same method as in table 3.

The measured and calculated values of $v_{\max }$ are also represented in the graph below, with smooth polynomial curves fitted to the data points.


Figure 20: Shows the calculated and the measured values of the maximum velocity.

It can be seen that the model's values are smaller by 4 to $5 \mathrm{~ms}^{-1}$, than the measured maximum velocities. The results of the zero litres rocket provide a correction of just the right magnitude (table 5). When the empty bottle was launched at the initial pressure of 1.6 bar it accelerated to 6 to $7 \mathrm{~ms}^{-1}$, which means if the rocket still has a 1.6 bar pressure inside it after the first stage, it can still accelerate despite of the absence of fuel. Therefore, the model can be improved by considering this accelerating force that causes the systematic error.

Table 5: Shows the experimental result of the zero-litre water rocket

| $0.0 / 12$ | Initial pressure: <br> $(1.6 \pm 0.2)$ bar | Water <br> amount: <br> 0 litre | $v_{\max }=$ <br> $(6.7 \pm 0.4) \mathrm{ms}^{-1}$ | $t_{t}=0 \mathrm{~s}$ | $h_{\max }=$ <br> $(2,42 \pm 0.02) \mathrm{m}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |

Note: The errors were calculated with the same method as in table 4.
iii. Determining the height reached by the rocket in the $1^{\text {st }}$ phase

In this experiment, the height $h_{1}$ reached by the rocket in the first stage was calculated by integrating (11) from $t=0 \mathrm{~s}$ to $t=t_{t}$, by a graphing software GeoGebra:


Figure 21: Shows the method of determining $h_{1}$ by integrating (11) from 0 to $t_{t}$ (shaded in table 6)

Table 6: Shows the calculated heights reached by the water rocket in the first phase

| Initial parameters |  |  |  |
| :---: | :---: | :---: | :---: |
| Mass of empty rocket $m_{R}=(0.225 \pm 1) \mathrm{g}$ |  | Density of water: $1000 \frac{\mathrm{~kg}}{\mathrm{~m}^{3}}$ |  |
| Average initial pressure $p_{1}$ : $\left.2.9 \pm 0.3\right)$ bar |  | Area of nozzle $A_{m}=(3.14 \pm 0.06) \mathrm{cm}^{2}$ |  |
| Amount of water (ml) | Calculated average of $u_{1}$ and $u_{2}, \bar{u}\left(\mathrm{~ms}^{-1}\right)$ | Calculated time $t_{t}(\mathrm{~s})$ | Calculated height in the $1^{\text {st }}$ phase $h_{1}$ (m) |
| Error: $\pm 5$ | Error: $\pm \approx 10 \%$ | Error: $\pm \approx 10 \%$ | Error: $\pm \approx 10 \%$ |
| 383 | 17.6 | 0.07 | 0.5 |
| 479 | 17.1 | 0.09 | 0.7 |
| 575 | 16.6 | 0.11 | 0.9 |
| 671 | 16.0 | 0.13 | 1.1 |
| 767 | 15.4 | 0.16 | 1.2 |
| 863 | 14.8 | 0.19 | 1.4 |
| 958 | 14.0 | 0.22 | 1.6 |
| 1054 | 13.1 | 0.26 | 1.8 |
| 1150 | 12.0 | 0.31 | 1.9 |
| 1533 | - | - | - |

## b) The phase when the rocket has run out of fuel

After the ejection of the water ends, the rocket still goes upwards with decreasing velocity. This is the second phase. At the beginning of this stage, the rocket has a mass of $m_{R}$ and a velocity of $v_{\max }$. Similarly, in this phase the two forces acting oppositely to the direction of the motion of the rocket are gravity $-m g$ and air drag $-C v$. To obtain the rocket's maximum height, first, the velocity of the rocket in this phase should be expressed.
i. Determining the height reached by the rocket

The motion of the water rocket in the second stage can also be understood by applying Newton's second law: $\sum F=m a$, which in this case is a first order inhomogeneous differential equation [11]:

$$
\begin{equation*}
-g=\frac{d v}{d t}+\frac{C_{v}}{m} v \tag{12}
\end{equation*}
$$

When $t=0^{8}$ the velocity of the rocket is $v_{\max }$. Using this initial condition, the velocity in the second phase can be expressed by solving the differential equation: ${ }^{9}$

$$
\begin{equation*}
v(t)=\left(v_{\max }+\frac{g}{k}\right) e^{-k t}-\frac{g}{k} \tag{18}
\end{equation*}
$$

Note: For more comfortable notations $\frac{C}{m}=k$.
After the time of rise $t_{f l y}$ to the highest point, the velocity of the rocket is $v=0$ for it rises until it stops. Using this condition, the time of flight is:

$$
t_{f y}=\frac{1}{k} \ln \left[\frac{k v_{\max }+g}{g}\right]
$$

To obtain the height reached by the rocket in the second phase $h_{2}$, equation (12) should be integrated, and to express the maximum height $h_{\max }$ it should be integrated from $t(0)$ to $t_{f l y}$ and the height of in the first phase $h_{1}$ should be added.

$$
\begin{gathered}
h_{2}=\int_{t(0)}^{t_{f l y}}\left(v_{\max }+\frac{g}{k}\right) e^{-k t}-\frac{g}{k} d t \\
h_{2}=\frac{1}{k}\left[-\left(v_{\max }+\frac{g}{k}\right) e^{-k t_{f l}}-g \mathrm{t}_{\mathrm{fly}}+V_{\max }+\frac{g}{k}\right]
\end{gathered}
$$

[^6]
## Calculating the maximum height

In this section, the same air drag coefficient ( 0.75 ) is used as in the Approximation of $C$ section in the appendix, which means the value of $k=0.04$.

| Initial parameters |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mass of empty rocket $m_{R}=(0.225 \pm 1) \mathrm{g}$ |  |  |  | The air drag coefficient $c=0.75$ |  |  |
| Average initial pressure $p_{1}$ : $\left.2.9 \pm 0.3\right)$ bar |  |  |  | Density of air $\rho_{\text {air }}=1.29 \frac{\mathrm{~kg}}{\mathrm{~m}^{3}}$. [9] |  |  |
| Largest cross-sectional area$A_{L}=(80.1 \pm 0.5) \mathrm{cm}^{2}$ |  |  |  | Value of $k=0.04$ |  |  |
| Water and bottle volume ratio | $\begin{gathered} V_{0} \\ \text { (litre) } \end{gathered}$ | Calculated from model |  |  |  | Measured <br> $h_{\max }(\mathrm{m})$ <br> from table <br> 2 |
|  |  | $t_{f l y}(\mathrm{~s})$ | ```Height in the 1 st phase hi (m) from table 6``` | Height in the $2^{\text {nd }}$ phase $h_{2}$ (m) | Calculated maximum height $h_{\text {max }}=$ $h_{1}+h_{2}(\mathrm{~m})$ |  |
|  | $\begin{aligned} & \text { Error: } \\ & \pm 0.005 \end{aligned}$ | $\begin{aligned} & \text { Error: } \\ & \pm \approx 10 \% \end{aligned}$ | $\begin{aligned} & \text { Error: } \\ & \pm \approx 10 \% \end{aligned}$ | $\begin{aligned} & \text { Error: } \\ & \pm \approx 10 \% \end{aligned}$ | Error: $\pm \approx 10 \%$ | Error: $\pm 0.5$ |
| 0.17 | 0,383 | 1.66 | 0.5 | 13.9 | 14.4 | 16.2 |
| 0.21 | 0,479 | 1.84 | 0.7 | 16.9 | 17.6 | 18.6 |
| 0.25 | 0,575 | 1.96 | 0.9 | 19.3 | 20.2 | 18.6 |
| 0.29 | 0,671 | 2.04 | 1.1 | 21.0 | 22.1 | 21.9 |
| 0.33 | 0,767 | 2.09 | 1.2 | 21.9 | 23.1 | 21.8 |
| 0.38 | 0,863 | 2.1 | 1.4 | 22.1 | 23.5 | 23.1 |
| 0.42 | 0,958 | 2.07 | 1.6 | 21.5 | 23.1 | 23.6 。 |
| 0.46 | 1,054 | 1.99 | 1.8 | 19.9 | 21.7 | 21.9 |
| 0.50 | 1,150 | 1.83 | 1.9 | 16.9 | 18.8 | 17.8 |
| 0.67 | 1,533 | - | - | - | - | 8.5 |

Table 7: Shows the variables needed to determine the maximum height that the water rocket can reach

Figure 22: Shows the calculated and the measured values of the maximum height reached by the water rocket at the initial pressure of 2.9 bar


The heights calculated from the model fit the measured heights very well. The maximum of each curve, as read from the graphs, occurs at $0.37 \pm 0.02$; which is the optimal volume ratio of the water and bottle.


## IV. CONCLUSION



In spite of the large uncertainty in the initial pressure, the model is able to predict the optimal volume ratio of water and bottle $0.37 \pm 0.02$, which is also obtained by experiment.

However, the hypothesized value of $\frac{1}{3}=0.33$ and $40 \%=0.40$ to $50 \%=0.50$ does not lie within the interval $0.37 \pm 0.02$, therefore, the statements that the optimal value is $\frac{1}{3}$ or between $40 \%$ and $50 \%$ of the volume of the bottle are not justified by the experiment. It is only acceptable as a rough estimation.

The applicability of the model is limited to the case when all the water leaves the bottle by the end of the first phase of the movement of the rocket. In addition, the model can be refined by considering the effect of the acceleration caused by the air coming out or the variation of the mass by changing the weight on the nose of the rocket.


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## VIII. Appendix


a) The unrounded values of the experimental results produced by Logger Pro:

| The average initial pressure $p_{1}:(2.9 \pm 0.3)$ bar |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| The ratio | Initial water amount <br> $V_{0}(\mathrm{ml})$ | Maximum velocity <br> $v_{\max }\left(\mathrm{ms}^{-1}\right)$ | Time of <br> ejection of <br> water $t_{t}(\mathrm{~s})$ | Maximum <br> height $h_{\max }(\mathrm{m})$ |  |
|  | error: $\pm 5 \mathrm{ml}$ | error: $\pm 1.14381 \mathrm{~ms}^{-1}$ | error: $\pm 0.0034$ | error: $\pm 0.5 \mathrm{~m}$ |  |
| $2.0 / 12$ | 383 | 21,08582 | 0,0704 | 16.2 |  |
| $2.5 / 12$ | 479 | 23.96376 | 0,0876 | 18.6 |  |
| $3.0 / 12$ | 575 | 25.98061 | 0,0875 | 19.7 |  |
| $3.5 / 12$ | 671 | 25.35379 | 0,1418 | 21.9 |  |
| $4.0 / 12$ | 767 | 26.03682 | 0,1293 | 21.8 |  |
| $4.5 / 12$ | 863 | 25.84454 | 0.1668 | 22.1 |  |
| $5.0 / 12$ | 958 | 26.57256 | 0,1793 | 23.6 |  |
| $5.5 / 12$ | 1054 | 24.76175 | 0,2023 | 21.9 |  |
| $6.0 / 12$ | 1150 | 21.04051 | 0,2544 | 16.8 |  |
| $8.0 / 12$ | 1533 | 10.77093 |  | 8.5 |  |
| $0.0 / 12$ | initial <br> pressure: <br> $(1.6 \pm 0.2)$ <br> bar | water <br> amount: <br> $0 l$ | $(6.743 \pm 0.3947) \mathrm{ms}^{-1}$ | 0 s |  |

Table 8: Shows the measured values of (table 2 and table 5)

## b) The approximation of $C$ :

$-C v(t)-m(t) g=\frac{d v}{d t} m(t)+\frac{d m}{d t} \bar{u}$, where $C$ depends on the density of air $\rho_{\text {air }}=1.29 \frac{\mathrm{~kg}}{\mathrm{~m}^{3}}$, the air drag coefficient $c$, and the largest cross-section of the rocket $A_{L}$.

Dividing the equation by $m(t)$ and rearranging it:

$$
\frac{d v}{d t}=-\frac{d m}{m(t)} \frac{\bar{u}}{d t}-g-\frac{\operatorname{Cv}(t)}{m(t)}
$$

This equation can only be solved numerically because both the mass and the velocity are changing with time, so the term of the air drag should be approximated to see how much it would vary in the maximum velocity.

Note: Since the rocket does not go really fast, an assumption can be made that the force of air drag is proportional to its velocity [9].

$$
d v \approx \int \frac{C v d t}{m(t)} \approx \int \frac{C v d t}{\left(V_{0-} \bar{u} A_{m} t\right) \rho_{w}+m_{R}}
$$

To solve the integral an assumption should be made that the mass of the rocket is not changing, so an arithmetic mean of the initial and the final mass should be used.

According to several articles and scientific investigations [1,5,6] the air drag coefficient can range from 0.2 to 0.75 . To see how much the air drag maximum influences the rocket's velocity in the first phase, the largest value for the velocity should be expressed:

$$
C=1.29 \times 0.75 \times 0.00801=0.01
$$

The arithmetic mean of the smallest mass (at $\frac{2.0}{12}$ ) is:

$$
\frac{\left(V \rho_{w_{0-}}+m_{R}\right)+m_{R}}{2}=\frac{1}{2} V_{0} \rho_{w}+m_{R}=0.192+0.225=0.417
$$

Since $C$ and the arithmetic mean of the mass are constants they can be brought out from the integral and the integral of the velocity is the height it reached in the first phase, which, according to the videos is at most 2 meters:

$$
\frac{0.01 \int v d t}{0.417}=\frac{0.01 \times 2}{0.417}=0.048 \mathrm{~ms}^{-1}
$$

This term of the equation can be neglected for it is much smaller compared to the measured maximum velocity of $16.8 \mathrm{~ms}^{-1}$ at $\frac{2.0}{12}$ from table 4 (shaded).

## c) The deduction of equation (7):

$$
\begin{align*}
& P(t)=v(t) m(t)  \tag{4}\\
& p(t+\Delta t)=(v(t)+\Delta v)(m(t)+\Delta m),  \tag{5}\\
& p_{w}(t+\Delta t)=-(\bar{u}-v(t)) \times|\Delta m|=\Delta m(\bar{u}-v(t)) \tag{6}
\end{align*}
$$

If equations $(4 ; 5 ; 6)$ are substituted into Newton's second law the equation looks like this:

$$
\begin{gathered}
F=\lim _{\Delta t \rightarrow 0}\left[\frac{(v(t)+\Delta v)(m(t)+\Delta m)+\Delta m(u(t)-v(t))}{\Delta t}\right] \\
F=\lim _{\Delta t \rightarrow 0}\left[\frac{v(t) m(t)+v(t) \Delta m+m(t) \Delta v+\Delta v \Delta m+\Delta m u(t)-v(t) \Delta m}{\Delta t}\right]
\end{gathered}
$$

After the algebraic simplifications the equation looks like the following:

$$
\begin{equation*}
F=\lim _{\Delta t \rightarrow 0}\left(\frac{m(t) \Delta v+\Delta m \Delta v+\Delta m \bar{u}}{\Delta t}\right) \tag{7}
\end{equation*}
$$

d) The deduction of equation (11)

$$
\begin{equation*}
-m(t) g=\frac{d v}{d t} m(t)+\frac{d m}{d t} \bar{u} \tag{8}
\end{equation*}
$$

After the division and the rewriting of the mass that it equals the volume of the water times the density of the water, the rearranged equation should look like this:

$$
\begin{equation*}
\frac{d v}{d t}=-\frac{\frac{d V}{d \iota} \rho_{w}}{V(t) \rho_{w}+m_{R}} \times \bar{u}-g \tag{9}
\end{equation*}
$$

From the assumption before, the rate of decrease of the volume of the rocket is:

$$
-\frac{d V}{d t}=\bar{u} A_{k}
$$

So, the rocket's volume at time $t$ is:

$$
V(t)=V_{0}-\bar{u} A_{k} t
$$

Substituting the volumes back to equation (9):

$$
\begin{equation*}
d v=\frac{\bar{u}^{2} A_{k} \rho_{w} d t}{\left(V_{0}-\bar{u} A_{k} t\right) \rho_{w}+m_{R}}-g d t \tag{10}
\end{equation*}
$$

Let the denominator, which is the mass of the rocket at time moment $t$, be y :

$$
y=\left(V_{0}-\bar{u} A_{k} t\right) \rho_{w}+m_{R}
$$

Expressing $t$ to determine $d t$ to substitute back to equation (10):

$$
\begin{gathered}
-\frac{y-m_{R}}{\bar{u} A_{k} \rho_{w}}-V_{0}=t \\
d t=-\frac{d y}{\bar{u} A_{k} \rho_{w}} \rightarrow d v=-\frac{d y}{y} \bar{u}-g d t
\end{gathered}
$$

After the definite integration of the equation from $t_{0}$ to $t$ and the substitution of $y$ and $y_{0}$ back to the equation, the velocity at any time $t$ can be expressed:

$$
\begin{equation*}
v(t)=v_{0}+\bar{u} \ln \left[\frac{V_{0} \rho_{w}+m_{R}}{\left(V_{0}-\bar{u} A_{k} t\right) \rho_{w}+m_{R}}\right]-g(t) \tag{11}
\end{equation*}
$$

## e) The deduction of equation (18)

The motion of the water rocket in the second stage applies Newton's second law: $\sum F=m a$, which in this case is a first order inhomogeneous differential equation:

$$
\begin{equation*}
-g=\frac{d v}{d t}+\frac{C}{m} v \tag{12}
\end{equation*}
$$

Note: The initial condition for this differential equation is when $t=0$ (the time $t=0$ means the beginning of the second stage and the end of the first stage) the velocity of the rocket is $v_{\text {max }}$.

To solve an inhomogeneous differential equation, first the homogeneous equation is solved and then add to a particular solution of the equation [11] which in this case is: $v_{\text {inhom }}=v_{\text {hom }}+v_{P}$

The homogeneous differential equation:

$$
\begin{equation*}
0=\frac{d v}{d t}+k v, \tag{13}
\end{equation*}
$$

where $k=\frac{c}{m}$.
The solution of (13) has to be sought in the form:
$v_{\text {hom }}=A e^{\lambda l}$, where $A$ and $\lambda$ is a constant and $t$ is time. Differentiating this equation will give:

$$
\frac{d v_{h o m}}{d t}=A \lambda e^{\lambda t}
$$

Substituting back to the homogeneous differential equation (13):

$$
\begin{equation*}
0=A \lambda e^{\lambda t}+k A e^{\lambda t} \tag{14}
\end{equation*}
$$

Simplifying this equation: $0=\lambda+k$, which follows:

$$
\begin{equation*}
\lambda=-k \tag{15}
\end{equation*}
$$

If (15) is substituted back to the equation (14), the homogeneous velocity should be expressed as:

$$
\begin{equation*}
v_{\text {hom }}=A e^{k t}=A e^{-k t} \tag{16}
\end{equation*}
$$

Now, a particular solution should be chosen:
If $\frac{d v_{p}}{d t}$ is chosen to be 0 then from the equation (12), $\frac{d v_{p}}{d t}+v_{p} k=-g, v_{p}=-\frac{g}{k}$ can be expressed so: $0+\left(-\frac{g}{k}\right) k=-g$

This follows that, $v_{\text {imhom }}=v_{\text {hom }}+v_{P}=A e^{-k t}+\left(-\frac{g}{k}\right)$
which means:

$$
\begin{equation*}
v(t)=A e^{-k t}-\frac{g}{k} \tag{17}
\end{equation*}
$$

Using the initial condition: the velocity is at maximum when $t=0$, to solve equation (17)
$v_{\text {max }}=A \times 1-\frac{g}{k}$
$A=v_{\text {max }}+\frac{g}{k}$
Substituting the value of $A$ back to equation (17) will give the velocity in the first phase at any time $t$ :

$$
\begin{equation*}
v(t)=\left(v_{\max }+\frac{g}{k}\right) e^{-k t}-\frac{g}{k} \tag{18}
\end{equation*}
$$

## Word counts:

All together: 4678
Tables: 658
References: 24
Equations, formulas: 6
The essay: 3990


[^0]:    ${ }^{1}$ From the experiment, it could be seen that the flight of a thin walled water rocket was very much unstable (not straight) than the older type. The older type mostly landed within a circle with a radius of three meter centered at the launch pad.

[^1]:    ${ }^{2}$ Unfortunately, the initial pressure could not be controlled as a constant very well, so an average had to be taken.

[^2]:    ${ }^{3}$ If the water column above the inner surface of the cork is assumed to be 1 litre (which is a little bit of an exaggeration) then the hydrostatic pressure is: 0.00314 bar, which is two orders of magnitude smaller than the error of the pressure readings.

[^3]:    ${ }^{4}$ If the final pressure is smaller than 1 bar, then there would be a negative number under the square root.

[^4]:    ${ }^{5}$ The deduction of the equation (7) is shown in the appendix.
    ${ }^{6}$ The air drag in this phase would slow the rocket by $0.048 \mathrm{~ms}^{-1}$ (calculated in the approximation of $C$ section in appendix.

[^5]:    ${ }^{7}$ The deduction of equation (11) is shown in the appendix.

[^6]:    ${ }^{8}$ The time $t=0$ means the beginning of the second stage and the end of the first stage.
    ${ }^{9}$ The deduction of equation (18) is in the appendix.

